

“Physicists are like 3% of rats.”

-Max Zolotorev, Lawrence Berkeley National Laboratory

If you have any questions, suggestions or corrections to the solutions, don't hesitate to e-mail me at dfk@uclink4.berkeley.edu!

Problem 1

(a)

As demonstrated in last week's problem set (problem 8), an ideal quarter-wave plate is described by a unitary Jones matrix. This means that the irradiance of the light beam is unaffected by traversing the plate. Also, the mirror is a perfect conductor, so 100% of the light is reflected. So the final wave's irradiance must be the same as the incident wave's.

(b)

The wave, initially polarized along the \hat{x} direction, first passes through the quarter wave plate, whose fast axis is oriented at -45° with respect to the initial light polarization:

$$\begin{bmatrix} E_x \\ E_y \end{bmatrix} = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 & -i \\ -i & 1 \end{bmatrix} \begin{bmatrix} E_0 \\ 0 \end{bmatrix} = \frac{E_0}{\sqrt{2}} \begin{bmatrix} 1 \\ -i \end{bmatrix} \quad (1)$$

Then the light bounces off a perfectly conducting mirror. This reverses the sign of the Poynting vector, which in turn changes the sign of the B-field relative to the E-field, since (as can be shown from Maxwell's equations):

$$\begin{aligned} \vec{E} &= E_0 \hat{\eta} e^{i(\vec{k} \cdot \vec{r} - \omega t)} \\ \vec{B} &= \frac{1}{v} \hat{k} \times \vec{E}, \end{aligned} \quad (2)$$

where $v = c/n$ is the phase velocity of light in a medium and $\hat{\eta}$ is the direction of the light's electric field. The light electric field undergoes a phase shift of π upon reflection (as can be deduced from the boundary conditions), but for circularly polarized light the direction of rotation (clockwise or counter-clockwise) of the electric field with respect to a fixed coordinate system is preserved. However, we are now viewing it from the opposite direction (since \vec{k} changed sign). Therefore the handedness of polarization has changed upon reflection:

$$\begin{bmatrix} E'_x \\ E'_y \end{bmatrix} = \frac{E_0}{\sqrt{2}} \begin{bmatrix} 1 \\ i \end{bmatrix} \quad (3)$$

This result can also be arrived at using Fowles's reflection matrix (page 52). The beam now passes back through the quarter waveplate, but now the wave sees the fast-axis oriented at $+45^\circ$. So we find that:

$$\begin{bmatrix} E''_x \\ E''_y \end{bmatrix} = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 & i \\ i & 1 \end{bmatrix} \cdot \frac{E_0}{\sqrt{2}} \begin{bmatrix} 1 \\ i \end{bmatrix} = -iE_0 \begin{bmatrix} 0 \\ 1 \end{bmatrix} \quad (4)$$

In other words the resultant light is linearly polarized in the \hat{y} direction.

Problem 2

First let's derive Fowles' result regarding the acceptance angle α for a fiber-optic cable (pages 46-47).

At the first phase transition as the light enters the fiber-optic cable, we have from Snell's law:

$$\sin \alpha = n_1 \sin \beta. \quad (5)$$

We want $\theta = \pi/2 - \beta$ to be greater than or equal to the critical angle, $\sin^{-1} n$ for total internal reflectance, where $n = n_2/n_1$. With a little trigonometry it can be shown that for these conditions,

$$\sin \beta = \frac{\sqrt{n_1^2 - n_2^2}}{n_1}. \quad (6)$$

Combining Eqs. (5) and (6) yields:

$$\sin \alpha = \sqrt{n_1^2 - n_2^2}, \quad (7)$$

which proves Fowles's assertion.

The next step is to compute the solid angle of light accepted by the fiber-optic cable, given by:

$$\Delta\Omega = \int_0^{2\pi} \int_0^\alpha \sin \theta d\theta d\phi = 2\pi(1 - \cos \alpha). \quad (8)$$

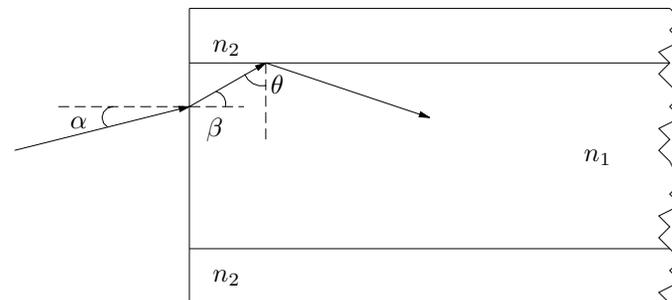


Figure 1

Divided by the total solid angle (4π), this yields the fraction T of the total light transmitted by the core to the end of the cable:

$$T = \frac{(1 - \cos \alpha)}{2}. \quad (9)$$

Problem 3

A vector field $\mathbf{F}(\vec{r})$ is equal to the curl of a vector potential $\mathbf{A}(\vec{r})$, so we know that the divergence of $\mathbf{F}(\vec{r})$ is zero:

$$\nabla \cdot \mathbf{F}(\vec{r}) = \nabla \cdot (\nabla \times \mathbf{A}(\vec{r})) = 0. \quad (10)$$

Then we know that:

$$\int \nabla \cdot \mathbf{F}(\vec{r}) dV = \oint \mathbf{F}(\vec{r}) \cdot d\vec{A} = 0 \quad (11)$$

Choose a volume of vanishing thickness $\vec{\delta}$ about a surface of area A (where $\vec{\delta}$ is always normal to the surface), then from Eq. (11) we have that:

$$\mathbf{F}_\perp(\vec{r} + \vec{\delta})A - \mathbf{F}_\perp(\vec{r})A + O(\delta) = 0 \quad (12)$$

where $O(\delta)$ indicates a term of order δ , which arises from some finite amount of “flux” of $\mathbf{F}(\vec{r})$ out the sides of the volume.

The condition for continuity of $\mathbf{F}_\perp(\vec{r})$ is that for each $\epsilon > 0$, there exists a $\delta > 0$ such that $|\mathbf{F}_\perp(\vec{r} + \vec{\delta}) - \mathbf{F}_\perp(\vec{r})| < \epsilon$. From Eq. (12) we know that:

$$|\mathbf{F}_\perp(\vec{r} + \vec{\delta}) - \mathbf{F}_\perp(\vec{r})| = \frac{O(\delta)}{A}. \quad (13)$$

Given any $\epsilon > 0$, clearly we can choose δ to make:

$$\frac{O(\delta)}{A} < \epsilon. \quad (14)$$

Therefore $\mathbf{F}_\perp(\vec{r})$ is continuous.

Problem 4

From Strovink’s treatment of reflection/refraction at a plane interface between insulators, we have for normal incidence:

$$\begin{aligned} \frac{E_r}{E_i} &= \frac{Z_2 - Z_1}{Z_1 + Z_2} \\ \frac{E_t}{E_i} &= \frac{2Z_2}{Z_1 + Z_2}, \end{aligned} \quad (15)$$

where E_r , E_i , E_t are the reflected, incident and transmitted electric field amplitudes, respectively, and

$$Z_{1,2} = \sqrt{\frac{\mu_{1,2}}{\epsilon_{1,2}}}. \quad (16)$$

In particular, for the ferromagnetic material described, $Z_2 \rightarrow \infty$ while Z_1 is finite, so:

$$\frac{E_t}{E_i} = \frac{2Z_2}{Z_1 + Z_2} \rightarrow 2. \quad (17)$$

Problem 5

(a)

Plane waves propagating in the $\pm z$ directions must satisfy Eqs. (15) at the interfaces ($z = 0$ and $z = L$). At either interface we have, since $Z_2 \rightarrow 0$,

$$\frac{E_t}{E_i} = \frac{2Z_2}{Z_1 + Z_2} \rightarrow 0. \quad (18)$$

Therefore \mathbf{E} vanishes in the material, i.e. $\mathbf{E}=0$ for $z < 0$ and $z > L$. So at the interfaces, $\mathbf{E}=0$.

The magnetic fields of the plane waves propagating in the $\pm z$ directions between the materials must satisfy $\mathbf{E}_+ \times \mathbf{H}_+ = -\mathbf{E}_- \times \mathbf{H}_-$ (i.e. the Poynting vectors of right- and left-traveling waves must be oriented in opposite directions). So while the electric fields cancel ($\mathbf{E}_+ = -\mathbf{E}_-$) at the interfaces the magnetic fields must add ($\mathbf{H}_+ = \mathbf{H}_-$)! Also we have the boundary condition $\mathbf{H}_\parallel = \mathbf{H}'_\parallel$, so that if \mathbf{H} is finite on one side of the interface, it must also exist on the other side. So there can be components of \mathbf{H} everywhere.

(b)

Our requirements from part (a) set up a standing wave, where the components of \mathbf{E} and \mathbf{H} are π out of phase. The wave is time independent in order to assure that $\mathbf{E}=0$ at the interfaces for all times t , so we can postulate:

$$\mathbf{E} = \vec{E}_0 \sin kz, \quad (19)$$

which works so long as $k = N\pi/L$ where N is an integer. So we get the condition on angular frequency from $k = \omega/c$, which implies

$$\omega = \frac{N\pi c}{L}. \quad (20)$$

Problem 6

We have two regions as shown in Figure 2, with k_1 and k_2 in each (defined as in the problem, where they are dependent on the potential V and the particle's total energy U , which is conserved, $U = T + V$). In region 1 we have the wavefunctions:

$$Ae^{i(k_1x - \omega t)} + Be^{-i(k_1x + \omega t)}, \quad (21)$$

and in region 2 we have a transmitted wavefunction:

$$Ce^{i(k_2x - \omega t)}. \quad (22)$$

Continuity of the wavefunctions across the boundary ($x=0$) demands:

$$A + B = C. \quad (23)$$

Since $\frac{\partial \psi}{\partial x}$ is also continuous:

$$k_1(A - B) = k_2C. \quad (24)$$

Substituting Eq. (23) into (24), we get:

$$\frac{B}{A} = \frac{k_1 - k_2}{k_1 + k_2} \quad (25)$$

If we assume $n \propto k$, then we get the formula for normal reflection of an EM wave at a dielectric interface with $\mu = \mu_0$:

$$\frac{B}{A} = \frac{n_1 - n_2}{n_1 + n_2} \quad (26)$$

Problem 7

Fowles 3.1

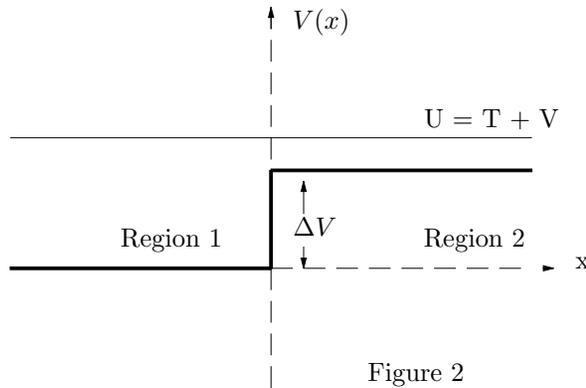


Figure 2

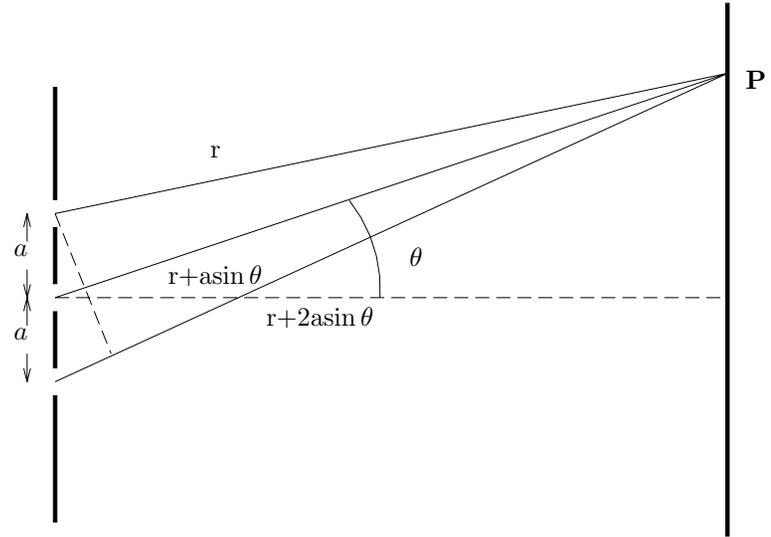


Figure 3

The sum of the amplitudes of the waves A coming from the slits at point P (see Figure 3) are given by the proportionality:

$$A \propto e^{ikr} + e^{ik(r+a \sin \theta)} + e^{ik(r+2a \sin \theta)} \quad (27)$$

or,

$$A \propto e^{ikr} (1 + e^{ika \sin \theta} + e^{2ika \sin \theta}) \quad (28)$$

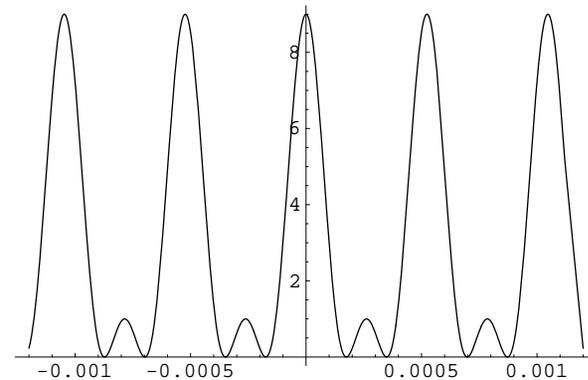


Figure 4

The interference pattern is given by the norm square of the amplitude:

$$I(\theta) \propto |A|^2 \propto (1 + \cos(ka \sin \theta))^2 \quad (29)$$

The pattern that you get when you plot this function depends on what value you choose for ka . Let's take $a = 1$ mm and $k = 12,000$ mm⁻¹, then our pattern is shown in Figure 4 as a function of θ .

Problem 8

Fowles 3.6

Light passes through the gas cell twice, so the optical path difference d_{op} is given by:

$$d_{op} = c\Delta t = \frac{2l}{c/n} - \frac{2l}{c} = 2l(n - 1) \quad (30)$$

n changes as the gas fills the cell, and since $I \propto 1 + \cos(2\pi d_{op}/\lambda)$, a new fringe appears every time $d_{op} = \lambda/2$. Thus the total number of fringes N is given by:

$$N = 2 \frac{2l(n - 1)}{\lambda} = \frac{4l(n - 1)}{\lambda}. \quad (31)$$

Plugging in the suggested values gives us $N = 203$ fringes.